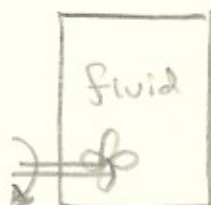


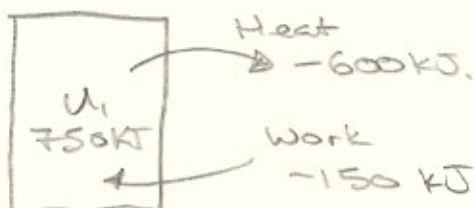
EX

given: a rigid tank with a paddle wheel is used to cool a hot fluid, shown. Initially, the internal energy of the fluid is 750 kJ. Due to the cooling process, the fluid loses 600 kJ. The Paddle wheel induces 150 kJ of work on the fluid.



REQUIRED: find the internal energy of the system. at the end of the cooling process

ANALYSIS: This system (fluid) is a closed system since there is no mass transfer across the boundary.



There is no mention of changes in KE & PE. so they can be neglected.

$$\Delta KE = 0 = \Delta PE$$

Recall:

$$Q_{12} - W_{12} = \Delta U + \Delta KE + \Delta PE$$

$$Q_{12} - W_{12} = \Delta U = U_2 - U_1$$

$$-600 - (-150) = U_2 - 750$$

$$U_2 = 300 \text{ kJ}$$

EX

GIVEN: An isolated rigid tank of volume  $0.2 \text{ m}^3$  contains air with an initial density of  $1.2 \text{ kg/m}^3$ . A paddle is used to transfer energy to the fluid at a constant rate of  $4 \text{ W}$  for  $20 \text{ min}$

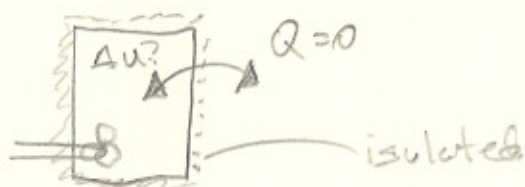
REQUIRED: Determine the internal energy of air in  $\text{kJ/kg}$

(A)  $\Delta U$

(B)  $\Delta u$

ANALYSIS: neglecting KE & PE

$$\Delta KE = \Delta PE = 0$$



$-4 \text{ W}$  for  $20 \text{ min}$

therefore to find total work, we multiply the rate of work by the time it is done.

$$\begin{aligned} W &= \dot{W} \cdot t \\ &= (-4 \text{ W}) \cdot (20 \cdot 60) \\ &= -4800 \text{ J} \end{aligned}$$

then we can use the first law of thermodynamics, where  $\Delta KE = 0$  and  $\Delta PE = 0$

$$\begin{aligned} Q - W &= \Delta U \\ 0 - (-4800) &= \Delta U \\ \therefore \Delta U &= 4.8 \text{ kJ} \end{aligned}$$

Part B.

$$u = \frac{U}{m}$$

$$\Delta u = \frac{\Delta U}{m}$$

$$= \frac{\Delta U}{\rho \cdot V}$$

$$= \frac{4.8 \text{ k}}{0.24}$$

$$= 20 \text{ kJ/kg.}$$

EX.

Calculate the changes of kinetic and potential energies of a system having mass of 2 kg whose velocity increases from 15 m/s to 30 m/s while the elevation decreases by 10 m at a rate of  $9.81 \text{ m/s}^2$ .

ANALYSIS:

$$\begin{aligned}\Delta KE &= KE_2 - KE_1 \\ &= \frac{1}{2} m v_2^2 - \frac{1}{2} m v_1^2 \\ &= \frac{1}{2} m (v_2^2 - v_1^2) \\ &= \frac{1}{2} (2) (30^2 - 15^2) \\ &= 675 \text{ J}\end{aligned}$$

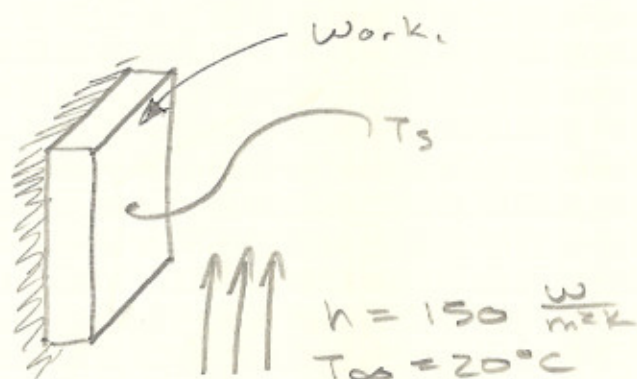
$$\begin{aligned}\Delta PE &= mgh \\ &= (2)(9.81)(10) \\ &= -197 \text{ J}\end{aligned}$$



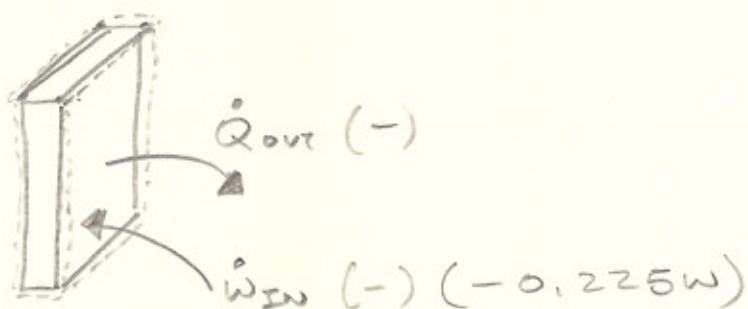
EX.

An electronic chip with dimensions  $5\text{mm} \times 5\text{mm} \times 1\text{mm}$  as shown, is embedded in a substrate. At steady state operation of the chip, the chip has an input of electrical power  $0.225\text{W}$ . The top surface of the chip is exposed to a cooling fluid, whose temp is  $20^\circ\text{C}$ , and an average heat transfer coefficient of convection of  $150 \frac{\text{W}}{\text{m}^2\text{K}}$ . If the heat transfer between the chip and substrate is negligible,

REQUIRED: Determine the surface temp of the chip in  $^\circ\text{C}$ .



ANALYSIS:



Application of the first law would be appropriate

$$\dot{Q} - \dot{W} = \frac{dE}{dt}$$

since the chip is in steady state there is no change in energy.

$$\frac{dE}{dt} = 0$$

$$\dot{Q} - \dot{W} = 0$$

$$\dot{Q} - (-0.225 \text{ W}) = 0$$

$$\dot{Q} = 0.225 \text{ W}$$

to the law of cooling.

$$\dot{Q} = -h A_s (T_s - T_\infty)$$

$$T_s = \frac{-\dot{W}}{h A_s} + T_\infty$$

$$= \frac{0.225}{(130)(25 \times 10^{-6})} + 20^\circ\text{C} = 80^\circ\text{C} = 353^\circ\text{K}$$

## SPECIFIC HEATS.

the spec heat is the energy required to raise 1 kg,  $1^\circ\text{C}$  ( $1^\circ\text{K}$ )

## TYPES OF SPEC HEAT.

Constant Volume:

$$C_v = \left( \frac{\partial u}{\partial T} \right)_v$$

Constant Pressure

$$C_p = \left( \frac{\partial h}{\partial T} \right)_p$$

$$\left( \frac{\text{kJ}}{\text{kg} \cdot ^\circ\text{C}} \right)$$

$$u(T, v)$$

$$h(T, p)$$

6.  
 $\Delta h, \Delta u, C_v, \& C_p$  FOR IDEAL GASES.

$$Pv = RT$$

it is known that an ideal

$$u = u(T)$$

we know that.

$$h = u + pv$$

$$h = u + RT \Rightarrow h(T) \text{ for an ideal gas.}$$

so that

$$C_{v0} = \left( \frac{\partial u}{\partial T} \right)_{v_0} \quad ; \quad C_{v0} = C_{v0}(T)$$

$$C_{p0} = \left( \frac{\partial h}{\partial T} \right)_{p_0} \quad ; \quad C_{p0} = C_{p0}(T)$$

for a process when an ideal gas changes from state 1 to state 2,  $\Delta u$  &  $\Delta h$  during the process can be obtained by

$$\Delta u = u_2 - u_1 = \int_1^2 C_{v0}(T) dT$$

$$\Delta h = h_2 - h_1 = \int_1^2 C_{p0}(T) dT.$$

REMARK: To carry out the integrations, relations  $C_{v0}$  and  $C_{p0}$  as functions of  $T$ .

$$C_{p0} = C_{v0} + R.$$

Another Ideal Gas property is the specific heat Ratio

$$K \equiv \frac{C_{p0}}{C_{v0}}$$

if  $K$  is not sig  $K \approx \text{Constant}$